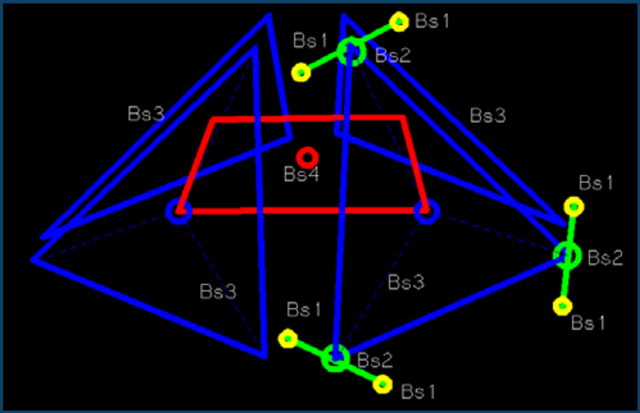
Determining Planetary Spin and Musical Gravitation in the Spheres of Cosmic Systems of Perfect Numbers

The Architecture of God



Hossam M. K. Aboulfotouh

Cairo - Egypt
2004

Part of the Architecture of God
on
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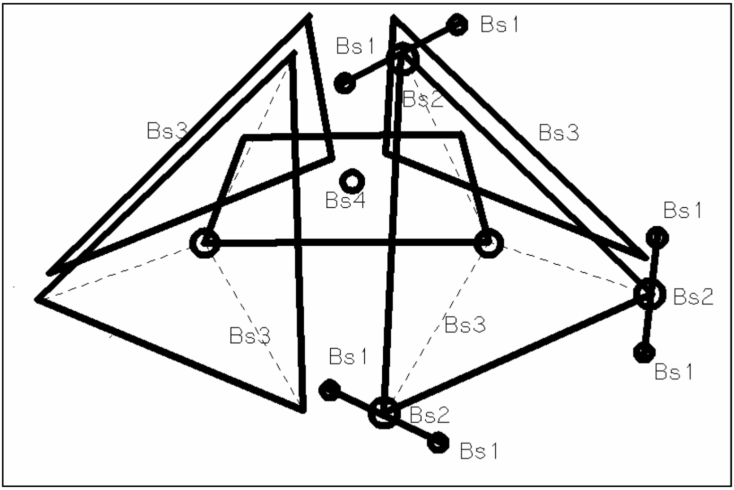

Hossam M. K. Aboulfotouh

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Determining Planetary Spin and Musical Gravitation in the Spheres of Cosmic Systems of Perfect Numbers

This work retrieves part of the first principles of the ancient Egyptian architectonic mathematics of material and ethereal cosmic systems of numbers in plane and spherical geometry, which are presented in thirty-nine mathematical equations.

It is part of the Architecture of God

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Dedication

To my son ***Mohamed****,*

To my daughters ***Amira*** *and* ***Ola****,*

To my ***family****,*

And

To the Victorious ***Egypt.***

H. Aboulfotouh at Bibliotheca Alexandrina

Preface

The first principles of the ancient architectonic mathematics of ethereal systems of numbers are sacred; and ancient civilizations did enquire about the philosophy of their first cause. This ancient realm investigates on the geometric laws of God, the ideas about creation, the structure of heaven, and the intrinsic attributes of the eternal ethereal substance. One of the subjects, deals with the laws that govern the correlation between two distinctive-types of orbits in a cosmic system of number, which were classified as, e.g., a divisible and the indivisible; the other and the same (or the one); or a diverse and the frame of reference. Simply, it is the correlation between any local orbit and the hosting sphere of the indivisible one. Medieval historians said that the Egyptian priests, e.g., Idris, studied the systems of numbers in order to understand the structure of heaven and the architectonic attributes of the material and ethereal systems of numbers. However, according to ancient traditions, and is still believed, revealing all laws about the systems of numbers implies that the scholar disobeys the commands of God. Hence, written Egyptian documents are nil, but the physical representation of the ancient Egyptian knowledge on this matter was designing pyramidal models of four sides. In later periods, those who did write about it, they either depicted the laws as dreams and revelations, or intentionally put them in improper mathematical sequence (chaos), targeting only those who will be interested to know, and have the ambition to enter this realm and to rewrite some of its many ancient pages from the beginning. The ancient notion is simply that, sets of numbers from one to six, to twenty-eight, to one thousand, or to as one is able to count, provide the seeds for constructing systems of numbers in multi-dimensions. The ancient approach, that is presented and mathematically retrieved in this work, relies on that the cosmic enclosure is similar to a ball that contains material bodies swimming in a compressed ethereal substance. In a dialogue of *Plato*, *Timaeus* the Italian scholar from Locris, who most likely studied in Egypt said, "God took the three elements of the same, the other, and the essence, and mingled them into one form, compressing by force the reluctant and unsociable nature of the-other into the-same". This ancient philosophy dealt with numbers as material or ethereal systems. Therefore, this work discuses the likely architectonic scenario of the evolution of cosmic-systems of numbers, such as probably, the observed solar systems or atoms, and perhaps the related unobserved ethereal systems, using merely the thrust-method of a megalithic arch. It shows that the architectonic structure and process of transformation of the perfect number system twenty-eight matches our solar system and the chromium atom. One might observe this work as it prove well stimulating to one's thinking, particularly if one has an interest to know, among other things, where life might exist in extra solar systems, i.e., the location of habitable zones, perhaps, in any system. Call this the alternative approach on how cosmic systems work without using the values of, e.g., mass, energy, or gravitation-constant in any equation. The numbers used in this work are not been chosen in a random way, nay, all key-numbers are part of those mentioned by the priests and philosophers of the ancient world concerning the ethereal systems in our cosmos. What is in between your hands, is part of the ancient wisdom about the secrets of number systems in nature. It is written in a numeric and geometric language that could be understood not only by those who did enquire about the secrets of the ethereal systems of numbers but also by those who are keen to know the other side of the truth from a mere architectonic perspective. It is part of the architecture of God.

Hossam M. K. Aboulfotouh

Contents

Introduction

Pythagoras proved that musical intervals could be characterized by numeric ratios and proclaimed that there is an analogy between planetary distances and musical intervals [1]. And, *Plato* [2] said that *Timaeus* explained how God created the numeric scale of musical intervals that upon which he structured the solar system and how its inner diverse-spheres (of the-other) are interacting with its outer sphere of the -same for conserving the perpetual motions of planets. However, *Plato*'s text lacks the mathematical principles that support the mentioned scenario; hence, the concept is still being trapped as a moral-paradigm until today. Similarly, the Pythagorean taxonomy, and perhaps magnifying, of perfect numbers is another intelligent but frozen concept that according to their definition [3,4], and that of Euclid [3,5] too, they disregarded, due to unknown reason, the relation between perfect numbers and the structure of material or ethereal cosmic systems. Or, perhaps, they followed the Egyptian tradition of not publishing the sacred secrets. On the other hand, in modern sciences, in General Relativity [6], *Einstein* introduced the postulation of curved space-time continuum; a gravitational field through which a planet will be in a continuous free fall around the sun. According to his theory, if most of the matter in the universe happens to be spinning, all of the space-time will be pulled around it [7]. However, why planets do spin with different cyclic rates, during the free fall is still unanswered question. Until today, there is no mathematical formula to explain the relation between the order of a celestial body, in terms of its equatorial radius, its orbit form and dimensions, and the cyclic rate of its spin. Recently, *Dones* and *Tremaine* have suggested that, huge Mars-size rocks may have caused Earth's rapid spin, i.e., from 200-hours-cycle into 24-hours-cycle; and, the larger the bodies that hit the Earth, the faster it will spin [8], which implies that spin might be the result of hits with no relation to a frame of reference. On the contrary, about twenty three centuries ago, most probably based on the ancient Egyptians and the *Pythagoras* philosophy, *Timaeus* said and *Plato* [2] confirmed that, "any body in the cosmos either material or ethereal, including the human body, works based on one law; that is the harmonic tuning between two orbits: a diverse and the-same, or the-one". Where a diverse is any local orbit in a cosmic-system and the-one or the-same is the outermost orbit of that system, which represents the frame of reference for all its local diverse orbits. In this ancient notion, all observed or hidden motions of all material or ethereal systems were seen as the result of this law.

Retrieving the architectonic mathematics that describe and determine the harmonic tuning between a diverse orbit (the-other) and the indivisible frame of reference (the-one or the-same), that it belongs to, is therefore the major goal and the core contents of this retrieving work. The methodology for realizing this aim is by determining mathematically two basic architectonic laws that were mentioned partly in ancient texts, such as those of the *Pythagorean* and *Platonic* philosophies. That is the ancient architectonic law of numbers and the ancient architectonic law of music of the spheres. Whereupon, and because the primary importance here is the motion in, and the stability of, the cosmic systems of numbers, this work also includes an attempt to determine a third architectonic law concerning the spin of orbs. Meanwhile, it aims to show what might was the ancient approach to the three architectonic laws of the evolution of cosmic systems and together were forming the ancient architectonic musical law of gravitation, that might was used for propelling and lifting heavy megalithic stones. In short, this is an endeavor to show that gravitation could be observed as the carrying workability of an orb, and spin could be observed as the orb's load transfer mechanism.

The methodology is primarily based on merely using the architectonic thrust-method in designing megalithic arches [9,10], e.g., the arches in Egyptian temples in Luxor or as that of Stonehenge in Salisbury. I think this most likely was the ancient method to understand the structure of a cosmic system and the motions of orbs, as I observe it encoded in designs of the Egyptian pyramids. Although this methodology differs from that of the realm of modern physics, scholars might detect that the laws of nature, particularly some of the general principles that were postulated in the Newtonian [11] Relativity [6,11], Quantum [12], and even Super string [11,13] theories, could be seen and think about in different way, via merely an ancient architectonic eye. This work does not speak about any of these great orthodox theories in relation to the retrieved ancient hypotheses, since it rather shows an entirely different approach on the architectonic laws of the structure of spherical-systems of numbers. In this work, I shall not use what do imply energy or a mass in reckonings, nor shall I speak about how a human being observes and records the motions of celestial bodies. This work focuses on part of the sacred ancient architectonic laws in plane and spherical geometry that ancient scholars said they describe, in a general way, the construction, stabilization, tuning, and sustaining of cosmic systems. It includes as well an abstract analysis on the motions of diverse (divisible) orbits and the indivisible frame of reference that occur due to only the applied-loads (and the corresponding compressive-stress) on the system under consideration. The idea is to substitute the applied-loads (lines of forces) with their corresponding travel-lengths in the periodic time of the system. Besides, by the end of this text, I shall try to determine, in relation to the escape velocities' application of the *Newtonian* law of gravitation [14,15], only the musical-tone (architectonic-frequency) and the corresponding diverse-thrust in the planet's system that to which the escape velocity might belong. It also shows the ancient architectonic view on the ethereal thrusts' propulsion scenario, in order to defy gravity. Despite that the hypotheses might seem strange and completely outside the mainstream of planetary theories, when testing its corresponding outputs of mathematical formulas based on using the data of NASA's planetary fact sheets [16a-d], and other sources [17,18], it may put these retrieved ancient philosophy in some right or possible perspective. The retrieved ancient laws do not challenge, or compete with, any of the modern theories; it is only an attempt to show that the ancient approaches such as those of the *Pythagorean* or *Platonic* schools of thoughts could be viewed outside the domain of myths. I hope that the readers view the retrieved ancient laws as a sort of simple explanation of at least one of the array of natural phenomena that were studied by the ancient scientific community, adding maybe a missing page in the book of ancient knowledge of man.

The hidden message of this work is that the laws that govern the structure of cosmic systems could also be related to the architectonic attributes and the carrying workability of these systems. That is, the celestial systems could be viewed as the outputs of the architectonic design-and-build laws of God (the supreme architect) where this work intends to highlight. Besides, by the end of this text, the reader might agree about that time may be only an idea in the observers' mortal minds who are hosted in one system of the cosmic enclosure. At the end, time might be seen as a product of motions that take place only within this system due to its compressive stresses; and outside the cosmic enclosure, all motions do stop and the idea about time dismantles.

Section-1.
The Architectonic Law of Numbers

One can observe numbers as material or ethereal systems that according to the scenario of their evolution the ancient Egyptians assumed that they are of two distinctive types: basic and complex. To portray this scenario, I propose the following architectonic image. A basic system-*Bs* may be at its primary state a heterogeneously elastic spherical body-(HESB) swims within a Euclidean plane that forms its steering ethereal structure-(SES). The size of HESB may be as tiny as one can imagine or the opposite, relative to the size of the beholder. Assume that SES is any plane in the cosmic enclosure. Due to reasons that will be discussed in section-2, SES is built from compressed ethereal fibers and any of its cross-sections is under a uniform compressive stress; thus, HESB will be under the effect of a uniform distributed load. As a mutual reaction, we can imagine that, HESB together with SES construct an ethereal protection-bearing ring around HESB, making it a nucleus of a ringed-system.

As in arched structures that are designed to bear only compressive stresses [9,10], within the middle third of this ring multi-paths of semi-elliptic thrusts would take place. The partial spread out of *Bs*'s ring will be as masonry-arches or the internal curved domain of megalithic-arches in ancient Egyptian temples or as the arches of *Stonehenge*, where the internal thrust of each is a parabolic curve, as shown in fig-1.

In a *Bs*, since the applied forces, due to the ring's structure property, are directed towards the nucleus of the ringed-system, the thrusts will be divided into two equal groups according to the direction of their motions: clockwise and anti-clockwise. These equalized, and opposite, motions keep the ring stationary. If SES contains other similar HESBs, under SES's compressive stress and HESBs' equal dominance, they may mutually compose a nucleus of one-ringed *Bs*. Since SES is not isolated from the rest of the cosmic enclosure, the ringed system may join with similar systems located in other planes (SESs) crossing its plane. Each HESB, therefore, will split into two, equally stressed, load-bearing elements: a spherical orb that runs on, and is steered by, a thrust, and a spherical pillar that remains in the system's nucleus. Here, I assume that the equatorial perimeter of an HESB equals the total sum of the equatorial perimeters of both an orb and a pillar. The orb will work as a roller-support (foundation) for carrying the nucleus of the *Bs* that swims in other SES (i.e., an orb is a male core, may be solid; a nucleus is a female hollow-sphere like a shield; and carrying is the ability and willingness to marry). It will join with one of the carried nucleus's pillars to form its central HESB. The load bearing state of a HESB, a pillar, an orb, or a *Bs*'s nucleus will be discussed in section-3, as a first principle for determining the spin of each.

For now, I shall imagine that the carrying ability or the "order" of a *Bs* denotes its name-number, which indicates the number either of its initial HESBs, its orbs, or its pillars. If the orbs are more than one in the ring, I presume that they distribute themselves at uniform distances on the ring's median circle, to be at the corners of concentric-shapes, but each of them runs on different thrust. This keeps a uniform distribution of the excess dynamic loads on the ring. The pillars may also follow the same distribution inside the *Bs*'s nucleus. Furthermore, I presume that the orbs of any *Bs* perform an equal cycle-length X (the thrust's perimeter) in the *Bs*'s periodic time T_b. Then, we can symbolize basic systems according to their name-numbers and carrying abilities as Bs_1, Bs_2, Bs_3, Bs_4, .. , and Bs_n.

Geometrically, the ring of a *Bs* that swims in a compressed cosmic enclosure is the equatorial plane of its ethereal protecting sphere, which matches the equator of the system's nucleus. For, I can presume that the structure and function of all latitude rings (parallel to the equatorial ring) are similar to the system's equatorial ring.

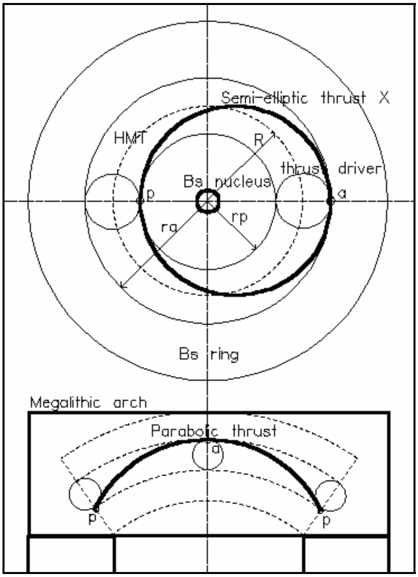

Figure-1: The parabolic thrust curve of a masonry or megalithic arch as a partial spread out of the ring's semi-elliptic-thrust of a *Bs*. The perihelion "p" and the aphelion "a" points denote the inner and outer limits of the middle third of an arch (doted) or a *Bs*'s ring that within which the thrust curve passes through in order that any cross section of them being under only a compressive stress. Due to that, a *Bs*'s ring has a harmonic attribute, the thrust driver's speed of self-rotation changes during the revolution.

Besides, imaginary, if tilted rings do exit, they will be of similar structure and function. Now, we can imagine that the common rule of rings of a system's sphere as follows. Since the ring's thrusts are semi-elliptic in shape, in case of a maximum permissible but compressive stress, the perihelion and aphelion of each thrust will be at the inner and outer limits of its ring's middle-third respectively. The location of these two limits are not identified on uniform distances as in masonry or megalithic structures [9,10] but, as will be discussed in section-3, it correlates to the harmonic architectonic frequencies of their vector-radii, due to the harmonic attribute of SES.

Furthermore, we can also imagine two circles generate the thrust curve, similar to those of the epicycloids curve [19], but this is a sliding case. The generating circle will be named as the thrust-driver; its center slides on the circumference of the median circle of the ring's harmonic-middle-third (HMT). The diameter's limits of the thrust-driver are the limits of HMT. As shown in fig-1, the thrust-driver performs two simultaneous cycles in T_b, either clockwise or anti-clockwise; i.e., its self-rotation around its center in diverse intervals and its orbiting cycle around *Bs*'s nucleus in equal sliding intervals.

Upon this, if the orbs of Bs_1, Bs_2, Bs_3, Bs_4 and Bs_n performed simultaneously one cycle in T_b, their total travel lengths will be *X, 2X, 3X, 4X,* and *nX,* respectively. Besides, when spreading out, in symmetrical way, half of HMT between the perihelion and aphelion points, half *X* will be its diagonal; and, despite the motion is in curve it jumps in linear increments; then, X could be reckoned using Eq.1:

$$X = 2 * \sqrt[2]{\left(\frac{\pi r_a + \pi r_p}{2}\right)^2 + \left(r_a - r_p\right)^2} \quad (1)$$

Where, r_a and r_p are the outer and inner radii of HMT, respectively; thus, r_a never approaches zero. For simplicity, we can hereafter put X equal $2\pi R$, where R is the HMT's mean-radius. On the carrying ability, logically the big carries the small, i.e., a *Bs* can carry only the systems below (or in special cases similar to) its order. For example, Bs_4 can carry four Bs_3 and their sub-systems: Bs_2 and Bs_1; but it cannot carry Bs_5.

Moreover, the joining of basic systems that have similar X size, generate a complex-system *Cs* in the cosmic enclosure. If Bs_4 carries four of Bs_3, then each of Bs_3 carries three of Bs_2 and each of Bs_2 carries two of Bs_1, they generate Cs_{28}. Its initial geometric form, at the joining moment, is a pyramid of four sides, see fig-2. It is assembled from 41 basic systems: 1 Bs_4, 4 Bs_3, 12 Bs_2, and 24 Bs_1. It contains 64 pillars and 64 orbs. Each loaded orb in the system together with one pillar of the nucleus it carries will create one HESB like Bs_1 at its primary-state. In Cs_{28}, they are 40 in total; 12 of them will be released out of the system after the joining process, leaving 28 HESBs as surplus for the system, as shown in fig-3. At the end, Cs_{28} will contain 24 orbs, 24 pillars, and 28 HESBs. The system's name-number is, therefore, the number of its surplus of HESBs. Its name-number may also be symbolized as Cs_{24+4}, where it implies the total sum of its Bs_1s and the order of its base Bs_4.

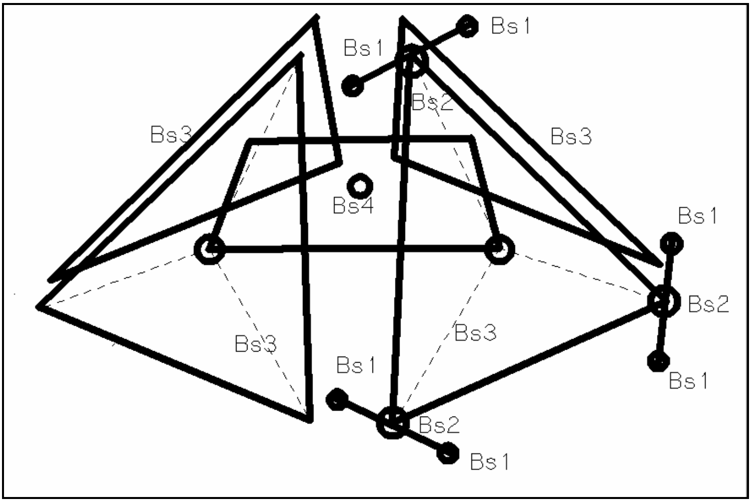

Figure-2: The initial pyramidal form of Cs_{24+4} during the assembling moment. The basic systems are not depicted in equal scales (sizes); and the thrust-X of each is not shown.

One can also observe the complex systems that are generated in this way as perfect number-systems, which have, at their initial states, symmetrical geometric-forms in the cosmic enclosure. The perfect number system Cs_{28} (or Cs_{24+4}) is generated numerically by: (1*2*3*4)+4+12-12=28. Similarly, the perfect number-system Cs_6 that is formed by only Bs_1, Bs_2, and Bs_3 is generated numerically by: (1*2*3)+3-3=6. The idea is how to reckon the remaining surplus of HESBs in the system after the joining process, taking into consideration that the HESBs of Bs_2s will be released out of the system during this process, so their quantity should be subtracted.

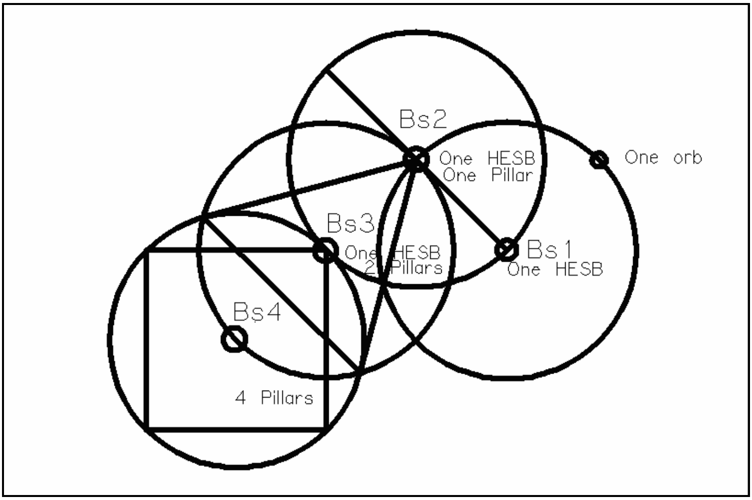

Figure-3: An imaginary projection plan shows the joining between the typical 4 basic systems of Cs_{24+4}. It shows one wing of the system. Presuming that Bs_4 is not carried by other system, its 4 pillars will remain without change. First, one of Bs_3's pillars will join with one orb of Bs_4 to form one HESB, thus each Bs_3 will have one HESB and 2 pillars; for four Bs_3s they will be 4 HESB and 8 pillars. Second, one of Bs_2's pillars will join with one orb of Bs_3, thus each Bs_2 will have one HESB and one pillar; for 12 Bs_2s they will be 12 pillars, and the 12 HESBs that will be released out of the system. Third, the pillar of Bs_1 will join with one orb of Bs_2; thus, each Bs_1 will have one HESB and its orb will remain; for 24 Bs_1s, they will be 24 HESBs.

On this account, it should be noted here that, the other methods that are introduced by the later *Pythagorean* [3,4] on how to generate a perfect number lack the purpose; as they did not observe numbers as physical systems. Or perhaps they followed the Egyptian traditions of never talk about the secrets of sacred knowledge. The definition of Euclid [3,5] and the later mathematicians[3,20], e.g., a perfect number is that equal to its aliquot parts, is only one of the cases of complex systems, that were dealt with in an abstract numeric way.

The formula for generating the structure number of any *Cs* that is assembled by four different orders of basic systems, in which Bs_1 is a necessary input, is:

$$Cs_n = (1*i*j*k)+ k+ (j*k)- (j*k) \qquad (2)$$

If *i* and *j* are always 2 and 3, respectively, and *k* is any even number from 4 to less than 360, the system's initial form will always be a pyramid, and transforms to a cone when *k* approaches 360 or more. That is, Cs_{24+4} is the first pyramid of a square base and $Cs_{2160+360}$ is a cone. Both Cs_{28} and Cs_{2520} were respected systems in ancient Egypt, which represent the beginning and the end of pyramidal transformations in the cosmic enclosure. There are other types of number-systems that have entail symmetric forms like a wheel, e.g., Cs_{1560}

that is generated numerically by: (1*3*17*30)+30+510-510=1560.

Architectonically, we can imagine that the initial forms of some atoms and solar systems are similar to perfect number-systems, taking into consideration that the retrieved scenario of complete evolution of the complex systems will be discussed in detail in section-2. For this, I shall presume that, in atoms, the number of their systems is the number of their neutrons, i.e., the surplus of HESBs. However, from this perspective, a Hydrogen atom matches Bs_1; and one can assume that its initial state is a neutron, as beta decay generates the main components of a Hydrogen atom [14,21]. Perhaps, at the scale of atoms, the rest of basic systems are unobserved because their lifetime is too short. Cs_{28} (or Cs_{24+4}) matches the Chromium atom, where in this case, its 24 pillars are similar to the protons and its 24 orbs are similar to the electrons. In addition, Cs_6 matches the Carbon atom.

One can also imagine that, many of the known atoms are like imperfect number systems. During the assembling process of a *Cs* (e.g., an atom), if any of its Bs_1s carried another Bs_1, it increases its HESBs (e.g., neutrons). Similarly, if any of its Bs_2s carried another Bs_2, it increases both its orbs (e.g. electrons) and its pillars (e.g., protons). In both cases, the system will be imperfect; similar cases generate the array of imperfect systems similar to the isotopes. In some complex systems, however, the process of increasing their HESBs, due to the excess loads of $Bs_{1}s$, transforms the system's HESBs again into a perfect state, i.e., uniform distribution and symmetry. An example is Cs_{117} (or Cs_{104+13}) that matches the Platinum atom. It is similar to the perfect number-system Cs_{117} that could be generated numerically as follows: (1*2*4*13)+13+52-52= 117. Besides, radioactive elements may be seen similar to the complex systems that are still in the process of releasing the HESBs of their $Bs_{2}s$, either in assembled or disassembled forms.

Now, I think, for reasons will be discussed in the coming sections, that the giant size of Cs_{28} matches our solar system. These sections include discussions on the complete evolution of this giant system, from its initial pyramidal form into becoming one multiringed-system, and on its intrinsic attributes: its architectonic musical law and its diverse to one-same tuning law. I shall call it hereafter as $Cs_{24+4.}$

Section-2.
The Architectonic Law of Music of the Spheres

In the beginning, I shall presume that each *Bs* has a module of rotation; it is the smallest thrust contour in the system's ring. It takes place within the system's nucleus, since the ring starts actually from the center of the system, like a disk. Second, I shall presume too that the perimeter M_b of a module of rotation is the system's measurement unit. Then, as a general condition, and for some reasons will be discussed in section-3, any point on any thrust that is less than X in the system's ring travels the same distance X in T_b. Then, while the orbs, or any point on the thrust X, perform(s) one simultaneous cycle in T_b, the module M_b performs several cycles, i.e., M_b, as the smallest thrust, is the cyclic unit of X. Therefore, the imaginary architectonic cyclic frequency ω_b of a *Bs* is given by Eq.3.

$$\omega_b = \frac{X}{M_b} \qquad (3)$$

Since the applied compression forces are uniform and perpetual, ω_b is harmonic, and since M_b is the system's unity, ω_b equals X. In unloaded *Bs* that carries only the external compression forces, its own semi-elliptic thrust-X represents, geometrically, the length of the actual load that the system's nucleus carries. If the thrust-X is being transformed into one concentrated load that applies directly on the system's nucleus, it will represent a load vector R_Z that equals in magnitude and travel length to that thrust X. Besides, if R_Z is used as a radius, it identifies the circular perimeter P_Z of the system's limit of zero-load[i], as shown in fig-4. Under any circumstance, the nucleus of unloaded *Bs* does not carry any external loads beyond this limit. Since the load vector R_Z equals X, we can also observe ω_b as the architectonic cyclic frequency of R_Z. Eq.3 may also be used to get the architectonic frequencies for different load vectors less than R_Z in a *Bs*, presuming that any of them is X of a separate system having the same M_b size. Thus, the lower (small) the radius the lower is its frequency. However, due to that any lower (small) load vector is part in the system, the lower the radius the higher the load, and accordingly the higher the orbiting velocity. If we imagine that R_Z is a high-rise building, where its foundation is the system's nucleus, in structure design, the load on a column in the sixth floor is more than that on the same column in the thirteenth floor and the load will be

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[i] Empirically, in the rock medium of megalithic structures, the angle of load refraction away from the canter of an arch is about 60^o; here, in an ethereal medium, if R=1, I presume that the maximum load refraction angle = *Atan* $(2\pi R)/(R/2)$= *Atan* 4π = 85.45^o

zero at the roof of this building. Thus, ω_b as an imaginary architectonic frequency indicates the harmonic level (tone) that upon which the load will be identified.

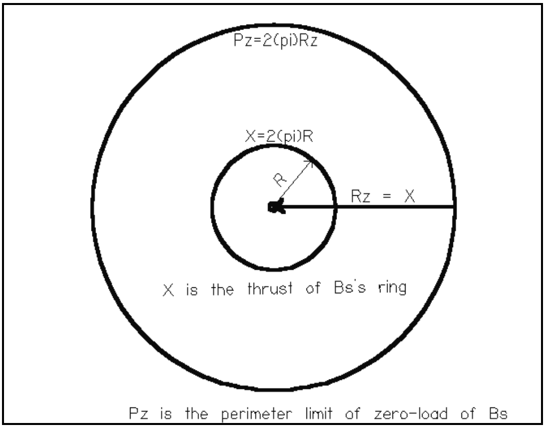

Figure-4: The main architectonic components of a basic system. The thrust-*X* in an abstract circular shape and the load vector R_Z that equals *X* and identifies the perimeter limit of zero-load of a basic system.

In complex systems, the case is quit different. If the 64 orbs of Cs_{24+4} performed simultaneously in T_b one cycle around their nuclei, due to the four directional motions of Cs_{24+4}'s sub-basic-systems, the actual collective load vector R_{Zc} that applies on the nucleus of the system's base "Bs_4" is given by Eq.4.

$$R_{Zc} = X * 2X * 3X * 4X = 24X^4 \qquad (4)$$

Eq.4 is based on that R_Z of each *Bs* works as a force that generates a moment (turning force) on the nucleus of the *Bs* that caries it. We can imagine that the nuclei of Bs_1, Bs_2 and Bs_3 are carried on the limits of zero-loads of Bs_2, Bs_3, and Bs_4 respectively, as shown in fig-5.

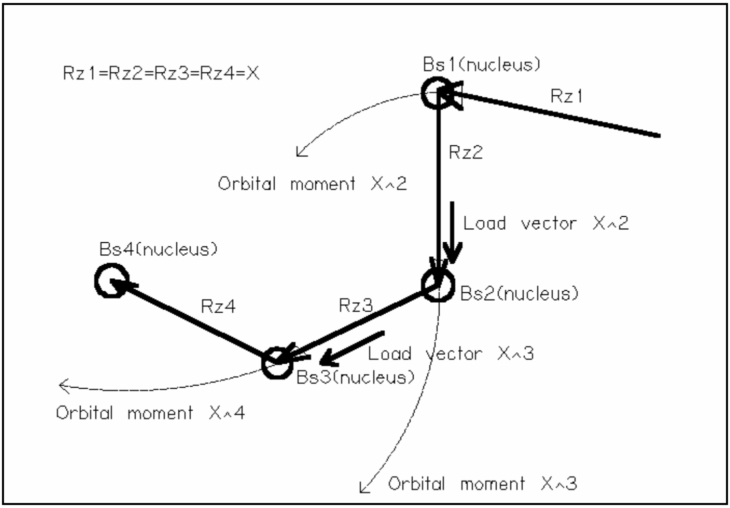

Figure-5: The carrying workability of one of the 24 wings of Cs_{24+4}. It shows the generated orbital moments: X^2, X^3, and X^4 around the nuclei of Bs_2, Bs_3, and Bs_4 respectively during one cycle per the periodic time T_b of a *Bs*.

Then, R_Z of Bs_1 will generate a moment equal to X^2 on Bs_2's nucleus. This moment is similar to an orbital thrust around Bs_2's nucleus. It represents the actual load that applies on it. This load may be transformed into a load vector that generates a moment equal to X^3 on Bs_3's nucleus. Similarly, the load vector of the moment X^3 generates a moment equal to X^4 on Bs_4's nucleus. For the 24 wings of the system, the collective load vector R_{Zc} equals $24X^4$; R_{Zc} as a radius identifies the perimeter limit of zero-load P_{Zc} of Cs_{24+4}.

In other words, geometrically, as shown in fig-6, repeating X during the system's four directional motions generates R_{Zc}; where it is the total sum of thrusts' images that encoded itself in multi cross-sections of the cosmic enclosure. For each Bs_1, repeating its X along Bs_2's X gives X^2; then repeating X^2 along Bs_3's X gives X^3, and finally repeating each unit layer of X^3 (each like X^2) along Bs_4's X gives X^4. For the 24 wings, the total sum of repeated images will be $24X^4$. Here, $24X^4$ is the real encoded volume of Cs_{24+4}'s architectonic structure that its-observed volume equals only $48X^3$.

Moreover, since basic systems, of similar X size, generate Cs, the imaginary architectonic frequency ω_x of Cs_{24+4}'s limit of zero-load R_{Zc} will also be X, where M_b is its module and that from Eq.4 is given by Eq.5.

$$\omega_x = X = \sqrt[4]{\frac{R_{Zc}}{24}} \qquad (5)$$

Unlike Eq.3 that deals with ω_b as the product of a single directional motion of *Bs*, Eq.5 deals with ω_x as a product of the four directional motions of Cs_{24+4}'s sub-basic systems. Since, ω_b of basic systems is harmonic, ω_x is also harmonic.

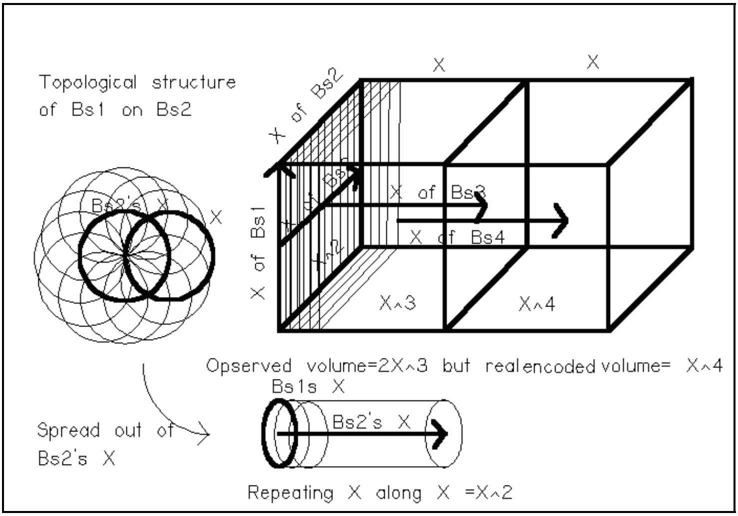

Figure-6: The linear model of the encoded images of thrusts for one-wing in Cs_{24+4} that will be generated during one cycle/T_b. The observed volume of one wing is only $2X^3$, however its real encoded volume is X^4. For the 24 wings of Cs_{24+4}, the observed volume will be $48X^3$, and the real encoded volume is $24X^4$.

Eq.5 may also be used to get the architectonic frequencies of different radii or load vectors less (lower) than R_{Zc} in Cs_{24+4}. Thus, we can put it in the form of Eq.6.

$$\omega_d = \sqrt[4]{\frac{R_d}{24}} \qquad (6)$$

Where, R_d is any radius in Cs_{24+4} that differs[ii] from R_{Zc}, and ω_d is the architectonic frequency of that different radius.

Furthermore, right after the joining process, I presume that the architectonic structure of Cs_{24+4} will transform, in topological manner, into a multi-ringed-system with one nucleus and multiple protecting rings around it. This transformation will take place within the system's limit of zero-load $P_{Zc}=2\pi R_{Zc}$, while conserving its architectonic frequency ω_x that represents its main intrinsic property. Then, P_{Zc} will be the circumference of the system's outer ring.

I shall also presume that Cs_{24+4}'s rings will be 46 in total; and they have the following sequence from the nucleus: 4 rings correspond to Bs_4, one ring gap, 12 rings correspond to Bs_3s, one ring gap, 24 rings correspond to Bs_2s and 4 rings as a cover for the system since it has a fourth order base. Bs_1s will not build rings, as their orbs will sail in the rings of Bs_2s.

[ii] In ancient terminology, R_d is radius of the-other, or radius of a diverse local orbit; and R_{Zc} is radius of the-same (one), or radius of the outer orbit of the system.

Besides, due to the harmonic attribute of the system, I presume that the two-limits of each of the 46 rings will match the limits of diatones (half tones). Taking ω_d of the mean radius of the system's nucleus as the first musical tone for the diatones of the system's rings, the musical tone "ω_x" of R_{Zc} will denote the system's musical name. Moreover, since musical octave contains 12 diatones [22a,b] and its second harmonic is twice its first harmonic [14], the ratio l between the frequencies of two successive diatones is 2^{-12}, i.e., l= 1.059463094 approximately.

In music, the typical musical octave starts from the note *C* or *Do* [22a]; however, a musical octave may start from any note [22b], e.g., from "A_2" or La_2= 110 cycles/second to its second harmonic La_3 = 220 cycles/second. The symbols of the 12 musical notes of an octave are *A, A#, B, C, C#, D, D#, E, F, F#, G, and G;* where they mean *La, La#, Si, Do, Do#, Re, Re#, Mi, Fa, Fa#, Sol,* and *Sol#,* respectively. The symbol # means major.

If M_b of our solar system is the decameter, according to NASA's planetary fact sheets [16a], our Sun's radius equals $0.695*10^8$ decameter. Then, using Eq.6, ω_d of our Sun's radius equals 41.25 cycles per T_b of X of our solar system. Accordingly, ω_x of R_{Zc} of our solar system equals $41.25*(l^{46})$= 588 cycles/T_b, which is equivalent to the note "D_4" or Re_4; it is the third harmonic [22] of D_2= 147c/s. In addition, using Eq.4,

R_{Zc} of our solar system is equal to 28,689*10^8 decameter (about 192AU or 192 R_d of Earth). Since ω_x equals X, it denotes the size of basic systems that might constructed our solar system, where it is based on the assumption of M_b's quantity. Using the multiple 10^4 to increase M_b's quantity, if M_b of our solar system is set as 10^4 or 10^8 of a decameter, the corresponding architectonic frequencies will be 1/10 or 1/100 of the mentioned notes respectively, while the size of X increases proportionally. In section-3, I shall identify the exact size of X of a system similar to our solar system.

Similarly, we can get the equivalent musical tone (architectonic frequency) of any radius in our solar system. The equivalent musical tone of Mercury's perihelion is close to La_2#= 117c/T_b. Venus's aphelion is close to Re_2= 147c/T_b. Earth's perihelion has a tone Re_2#= 157c/T_b. Mars's perihelion is close to Fa_2= 172 c/T_b. Jupiter's perihelion is close to La_3#= 234c/T_b. There is nearly one octave between Mercury's perihelion and Jupiter's perihelion; it is the first of the two musical octaves of Bs_2's rings of our solar system. The musical tone of earth's perihelion (Re_2#=157c/T_b) is nearly similar to that of R_{Zc} of the solar system (Re_4=588 c/T_b), i.e., life exists at two octaves below R_{Zc}. This might imply that, in any C_S, e.g., extra-solar systems, life may exist near to orbits with architectonic frequencies similar to that of R_{Zc} of these systems.

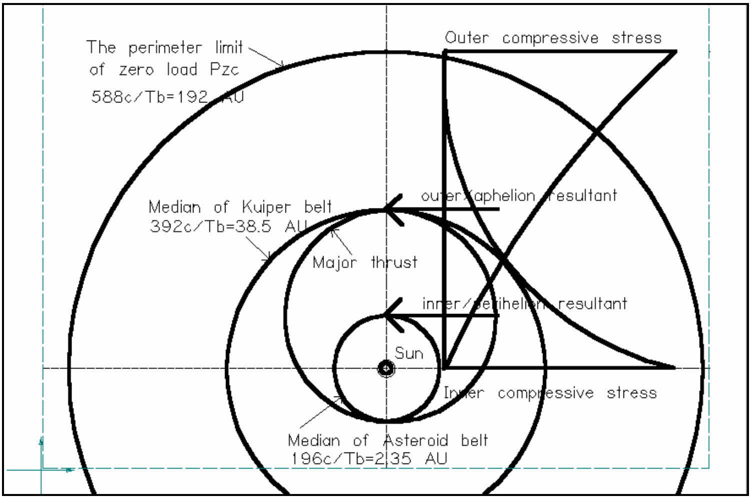

Figure-7: The two main resultants of the fluctuated compressive stress in Cs_{24+4}'s combined ring. For the maximum permissible load, due to that the ring is being under only compressive stress, the stress diagram for any of its cross sections will be only in the compression side. The resultant of each stress diagram for any cross section will denote the location of the thrust in that cross section. At the aphelion-point, the maximum compressive stress will apply on the outer limit of the ring with zero stress in the system's center. At the perihelion-point, the maximum compressive stress will apply on the center of the system, with zero stress in the outer limit of the ring. Due to that, the combined ring has multiple major-thrusts in its middle-third, its outer and inner circular-limits contain the array of the perihelion and aphelion points of these multiple thrusts. Thus the two resultants are in continues revolution and apply on any cross section of the combined ring denoting the two limits of its harmonic middle third. The compressive stress diagram of the ring's cross-section(s) is not linear, due to the harmonic distribution of loads.

If we imagine that the 46 rings form one combined ring (like a disk), the major architectonic thrust of the system will have a perihelion and aphelion at the inner and outer limits of the harmonic middle third of the combined ring. At these two limits, the two resultants of the fluctuated compressive stress diagrams [23] those apply on the cross section of the ring take place, as shown in fig-7.

In our solar system, the inner limit matches the median circle of the asteroid belt at ω_d= 588/3= 196c/T_b, and using Eq.4, its radius equals 354*10^8 decameter (354*10^6 km). The outer limit matches the median circle of the Kuiper belt at ω_d= 588*(2/3)= 392c/T_b, and using by Eq.4, its radius equals 5,667*10^8 decameter (about 38 AU). These two distances agree with the published data of both belts [16,17,&18]. Another reason that makes the inner limit (i.e., asteroid belt) the major disposal for Cs_{24+4}'s debris will be discussed in the following section.

Section-3.
The Architectonic Law of Spinning Motion

The following are the primary assumptions concerning the spin of orbs and nuclei of basic systems that I shall endeavor to prove it when discussing in details the spin of orbs and nuclei of cosmic number-systems, e.g., plants, natural-satellites, and the Sun of our solar system.

In an unloaded *Bs* that may carry the nucleus of other *Bs*, an orb of the first should thus be in the ready state to be able to carry the nucleus of the second and transfers its load to the thrust *X* of its home system. Normally, as I did presume earlier, an orb of a *Bs* travels actually on the thrust *X*, however, due to the harmonic process (in cycles) of load-transfer between two basic systems, it will carry a *Bs*'s nucleus that is located imaginary at the limit of zero-load of its home system. This means, the orb will transfer the orbital force of the moment that has been generated by the load vector R_Z of the carried system to the thrust *X* of its home system. This orbital force is, in fact, a thrust that matches the perimeter of zero-load P_Z of the carrier system; its perimeter equals $2\pi R_Z$ and T_b is its orbiting time-period, i.e., the thrust *X* and the orbital moment (P_Z) have the same angular velocity. The orb is then free to jump-outwards to P_Z of its system in a proper point in time in order to carry (join with) the other *Bs's* nucleus and together return back to the thrust that has a force-load equal to the load it carries (e.g., in this case it will be *X*). Then, the load of *X* will be the total moment that applies on the carrier-system's nucleus.

Furthermore, we can imagine that, as said earlier, geometrically in a *Bs*, the actual carrying load of any of its thrusts is the travel length that any point on these thrusts performs in T_b. In this case, the orb achieves its carrying workability via that, any point on the orb's equatorial thrust P_o (its domain and steering thrust) should travel a distance in T_b equal to P_Z that represents the load length it carried, and it was ready and able to carry. Accordingly, before and after carrying, the orb that is steered by its domain-thrust P_o performs several cycles α, in T_b, in order to transfer the load length P_Z to its thrust *X*; then and only then, it will be ready to perform the carrying job. Hence, we can say, the orb's spin α is a mechanism for load-transfer in T_b; and at that time, $\alpha * P_o = 2\pi R_Z = 2\pi X = P_Z$. Besides, since $\omega_b = X = R_Z$ of P_Z, we can say that the orb conserves ω_b in its carrying workability. Moreover, we can imagine that an *X* of a *Bs* is a P_Z of a minor thrust that its perimeter P_M equals *R*. During the ready state, if the orb runs on the orbit-thrust P_M, it carries only the load *X* and thus its spin in T_b will be S, where $S*P_o= X$, and $\alpha=2\pi S$.

We can also presume that an orb will spin with the same rate, according to its carrying load, disregard to the change in the tilt of its equatorial plane in relation to the equatorial plane of its *Bs*, because the load will not change. Besides, in unloaded *Bs*, e.g., Bs_1, that is carried by other system and it is in a condition that it does not carry any thing but itself, it is expected that, its orb will become in a state of rest or in a sleeping mood. In this case, the sleeping orb will not spin, and thus it will have a fixed orientation in relation to the system's nucleus while orbiting it similar to any point of the thrust-*X*.

Moreover, since both an orb and a pillar are equally stressed, the pillar carries also the orbital moment that is represented by P_Z during a ready state; thus, its spin α_p is given by: $\alpha_p*P_p= P_Z$, where P_p is perimeter of the pillar's domain equatorial thrust. On the other hand, the nucleus of unloaded *Bs* carries, in a ready state, the mean orbital load of the system, i.e., the orbital moment at the radius that has a mean architectonic frequency equal to $0.5\omega_b$, which equals $0.5X$; thus, the nucleus carries πX. Then, its spin α_n in T_b is given by: $\alpha_n*P_n= \pi X$, where P_n is the perimeter of the nucleus's domain equatorial thrust.

Now, in *Cs*, the case is more complex but amazingly organized and needs the following extended explanations and assumptions as first principles for establishing the spin equations of the actually loaded orbs of Cs_{24+4}. Following *Plato*'s definitions [2], in Cs_{24+4}, the perimeter of any of the inner rings' thrusts (or the thrusts of combined rings or parts of rings) will be named hereafter as "the perimeter of a diverse orbit" (P_d). The perimeter of the outer ring's thrust will be named as "the perimeter of the same" (P_X) where ω_x is the architectonic frequency of its radius. The thrust P_X may be a circle and matches the perimeter of zero-load P_{Zc}, if the difference between the frequencies of the inner and outer radii of its ring approaches but not equal zero. We can assume that the diatone of the system's outer ring is divided into micro-tones, where P_X is the thrust of the outermost micro-tonal ring.

Besides, any point on P_X performs one orbiting cycle in T_X, and any point on P_d performs one orbiting cycle in P_d 's local time-period T_d. An orb runs only on a P_d based on conserving ω_x of Cs_{24+4}'s R_{Zc}, which implies that, the orb that is orbiting the system's nucleus at any P_d should conserve the condition as if it is orbiting at the thrust P_X. Thus, it should perform several orbiting cycles K_{Vd} in T_X in order to travel a distance equal to P_X, i.e., $P_X = K_{Vd} * P_d$. This means that at any P_d, the orb's velocity V_d per T_X is constant, while its V_d is variable and has diverse quantities per T_d of each P_d. Moreover, each P_d of Cs_{24+4} is as X of Bs that has its own P_Z; i.e., $P_{Zd} = 2\pi P_d$. In Cs_{24+4}, P_{Zd} of any P_d is imaginary a product of a single motion; and on the contrary, P_{Zc} or P_X is the product of four directional motions. Besides, there will be a diverse thrust P_{dM} that its P_{Zd} matches P_{Zc} or P_X of Cs_{24+4}. Thus, P_{dM} will be the outermost median-thrust (load) between some perihelion and some aphelion for Cs_{24+4}'s orbs. Accordingly, as an example, in our solar system, its radius R_{dM} would be about 30.5 AU.

Since Cs_{24+4} is not isolated from the rest of the cosmic enclosure, some of its orbs may carry the nuclei of other systems. We can classify them in two types: a system-carrier-orb that carries Bs_n, and an ion-carrier-orb that carries only a Bs_1's base. Any orb of Cs_{24+4} should conserve ω_x in its spin, i.e., the spin α of an orb conserves the condition that any point on the orb's steering thrust travels a distance equal to P_{Zc} (or P_X) in T_X. However, as we shall see, each orb achieves this condition according to the type of load and the carrying workability.

We can also assume that the observed motion of a system-carrier-orb running on a P_d is, at most, the product of seven motions (6 + the motion of P_X) that we can divide into two groups of four motions, since the motion of a P_d participates with the two groups. I shall name Group-1 as the "steering mechanism" that links the spinning motion of an orb with the motion of its P_d. And, I shall name Group-2 as the "harmonization mechanism" that links the motion of a P_d with the motion of P_X, which conserves the condition: $P_X = K_{Vd} * P_d$. When taking into our consideration that, the motion of the frame of reference P_X is the product of the four directional motions of Cs_{24+4}, the observed motion of a system-carrier-orb is then the product of ten motions at most. In section-4, I shall add another one that makes them eleven motions in total.

Firstly, as shown in fig-8, Group-1 is composed of a P_d and one or two levels of steering-thrusts that have the same center of rotation, which is the center of the orb; i.e., they are carried on a P_d. Although we are speaking about semi-elliptic thrusts, each has only one center, which is the center of, an imaginary, sub-circular-ring that through which a thrust passes within its harmonic middle third HMT. We can imagine that the steering mechanism of any system-carrier-orb as multiple levels of thrust-contours that each level is composed from the three typical thrusts of a *Bs*: P_Z, X and P_M. The outer contour-level includes P_{Z3}, P_3, and P_{M3}; and the second inner level includes P_{Z2}, P_2, and P_{M2}, where the perimeter of any thrust, of any level, is equal to S times its comparable thrust in the contour level below it, i.e., $P_{Z3} = S * P_{Z2}$ and so on. It is similar to the correlation between X and P_o in Bs; besides, in this case both have the same center.

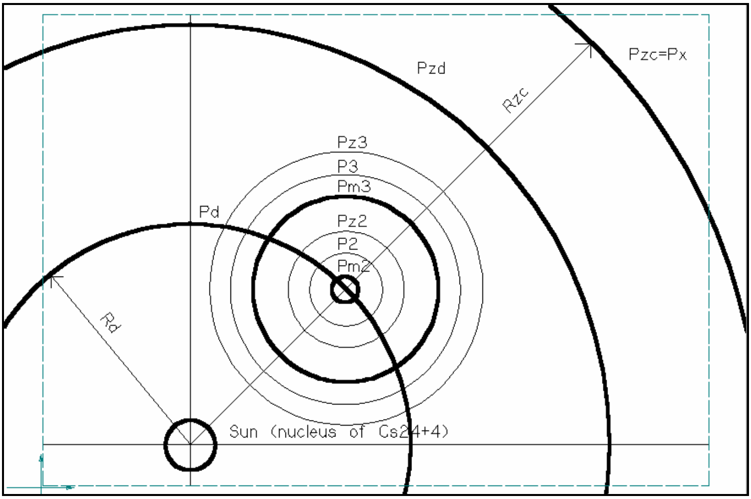

Figure-8: The thrust contour levels of the steering mechanism of a system-carrier-orb in Cs_{24+4}. They are carried on a diverse thrust P_d. In the ready state, these thrusts carry the orbital moment that applies at the perimeter of zero-load P_{Zd} of their P_d, and the latter carries the orbital moment at the perimeter of zero-load P_{Zc} of Cs_{24+4} (the perimeter of the same P_X). Their motions conserve the architectonic cyclic frequency ω_X of R_{Zc} of Cs_{24+4}.

The geometric perimeter of any of these thrusts can be reckoned using Eq.1; however, for simplicity I shall put them hereafter as Pz_3=$2\pi Rz_3$, P_3= $2\pi R_3$ and P_{M3}= $2\pi R_{M3}$, where Rz_3, R_3, and R_{M3} are their mean radii respectively, and similarly for the second inner level. As we shall see, it is expected that in most cases, e.g., in our solar system, loaded orb may take either P_{M3} or P_{M2} as a domain-thrust for the nucleus it carries; and related to the radius's architectonic frequency, of the P_d it chooses. However, in all cases, P_3 is the steering-thrust that to which the observed spin belongs. If P_{M3} was the domain-thrust, the inner contour-levels take place inside the carried nucleus, e.g., the planet.

Since, an orb is a foundation for other system's nucleus; we can presume that it has a working radius R_W, relative to its carrying state. In a solar system, R_W may equal the mean observed radius of the planet's equator. Or R_W may equal the radius of the planet's domain-thrust (R_{M3} or R_{M2}) or deviate from it with a factor Y; i.e., $R_{M3}= Y_3 * R_W$, or $R_{M2}= Y_2 * R_W$; where Y indicates the location of the planet's domain-thrust in relation to its actual working thrust P_W. If Y=1, the planet's P_W is equal to its domain-thrust, and then the planet's observed size follows the norm of Cs_{24+4}. However, if Y<1, the planet's domain-thrust is below its P_W and if Y>1, the planet's domain-thrust is above its P_W.

The steering mechanism achieves the condition that any point on the planet's working (but equatorial) thrust (P_W) travels a distance equal to P_d in T_d. Here we can presume that, P_d and the steering thrusts P_3 and P_2 are similar to the thrust-X of a Bs, where Pz_d, Pz_3, and Pz_2 are their perimeters of zero-load or their perimeters of the same. Accordingly, we can imagine that the steering mechanism works based on the following four conditions.

First, P_3 performs α cycles in T_d in order that any point on it travels a distance equal to P_{Zd}, where α=$2\pi S$, and S*P_3= P_d. Thus,

$$\alpha * P_3 = 2\pi * P_d \qquad (7)$$

Second, for an orb that takes P_{M3} as a domain thrust for the nucleus (planet) it carries.

$$P_3 = 2\pi * P_{M3} \qquad (8)$$

Third, for an orb that takes P_{M2} as a domain-thrust for the nucleus (planet) it carries, P_2 performs α cycles in T_d, similar to P_3's cycles, in order that any point on P_2 travels a distance equal to P_{Z3}, where α= $2\pi S$, and S= P_3/P_2= P_d/P_3. Thus,

$$\alpha * P_2 = 2\pi * P_3 \qquad (9)$$

Fourth,

$$P_2 = 2\pi * P_{M2} \qquad (10)$$

Then, by substituting the quantity of P_3 from Eq.9 in Eq.7, we get Eq.11.

$$\alpha^2 * P_2 = (2\pi)^2 * P_d \qquad (11)$$

In addition, by substituting the quantity of P_3 from Eq.8 in Eq.7 and substituting the quantity of P_{M2} from Eq.10 in Eq.11, we get Eq.12 and Eq.13, respectively.

$$\alpha * P_{M3} = P_d \qquad (12)$$
$$\alpha^2 * P_{M2} = 2\pi * P_d \qquad (13)$$

Then, if we inserted the factor Y in Eq.11, Eq.12, and Eq.13, and put the approximate quantities of P_d, P_2, and P_{M2}, we get the spin equations of Cs_{24+4}'s system-carrier-orbs.

$$\alpha * Y_3 * R_W = R_d \qquad (14)$$
$$\alpha^2 * Y_2 * R_W = (2\pi)^2 * R_d \qquad (15)$$
$$\alpha^2 * Y_2 * R_W = 2\pi * R_d \qquad (16)$$

Using the data in NASA's planetary fact sheets of our solar system [16b], I found that Eq.15 matches the case of Pluto, where its Y_2=1. Eq.14 matches the case of Jupiter, Saturn, Uranus, and Neptune, where Y_3 is nearly 1.0 for Jupiter and Saturn, Y_3=2.63 for Uranus, and Y_3=2.0 for Neptune. Eq.16 matches the case of both Earth and Mars, where Y_2 is 1.1 for Earth and 0.9 for Mars.

For Earth, α = 365.25 c/T_d, where T_X= K_{Vd}*T_d, and its S=58.13c/T_d. Since, $\alpha = 2\pi S$, Eq.16 may be put in the form: ($2\pi * S^2 * Y * P_W = P_d$), where $2\pi S^2 = K_\alpha$; and where K_α is the cycles that the thrust P_{M2} performs in T_d, i.e., $P_d = K_\alpha * P_{M2}$. This implies too, as the equatorial radius (or R_W) of Earth increases its spin reduces, for the same R_d. Besides, since P_3 is the major steering thrust, the observed spin is only α; the motion of both P_{M2} and P_2 is unobserved. The time of all steering thrusts is T_d, and the velocity of any point on any of them is constant and equals V_d of P_d of the planet.

Secondly, Group-2, or the harmonization mechanism, links the motion of a P_d with the motion of P_X. In between P_X and any P_d, I shall presume that there are two intermediate thrusts: P_E and P_F. Their mean radii are R_E and R_F respectively. In group-2, P_d, P_E and P_F are similar to P_{M2}, P_2 and P_3 in group-1 respectively; and P_X in group-2 is similar to P_d in group-1. Similarly, in group-2, V_d, S_d, and K_{Vd} are similar to α, S, and K_α in group-1, respectively; thus, in group-2, $V_d = 2\pi S_d$ and $K_{Vd} = 2\pi S_d^2$, *i.e.*, $V_d^2 = 2\pi K_{Vd}$. In this case, Group-2 has only one possible condition. The correlation between the motions of P_X and a P_d will be similar to Eq.16 of group-1, thus, in group-2, I imagine that P_X (or P_{Zc}) is as X of a *Bs* that has a P_Z, which is P_{ZX} that equals $2\pi P_X$. In our solar system, P_{ZX} equals 1,205 AU. Thus, Eq.17, Eq.18, and Eq.19 are similar to the equations of the first, the third, and the fourth conditions in group-1, respectively.

$$V_d * P_F = 2\pi P_X \qquad (17)$$

$$V_d * P_E = 2\pi P_F \quad (18)$$
$$P_E = 2\pi P_d \quad (19)$$

Now, by substituting the quantity of P_E from Eq.19 in Eq.18, and then from the generated equation substituting the quantity of P_F in Eq.17, we get Eq.20.

$$V_d^2 * P_d = 2\pi P_X \quad (20)$$

Then, we get Eq.21.

$$V_d^2 * R_d = 2\pi R_X \quad (21)$$

In addition, if we substitute each quantity of R_d from (Eq.14, Eq.15, and Eq.16) in Eq.21 and since $V_d^2=2\pi*K_{Vd}$, we get the three orbiting-spin-equations of system-carrier-orbs in Cs_{24+4} and as I previously identified for the planets of our solar system, they respectively are:

$$K_{Vd} * \alpha * Y_3 * R_W = R_X \quad (22)$$
$$K_{Vd} * \alpha^2 * Y_2 * R_W = (2\pi)^2 R_X \quad (23)$$
$$K_{Vd} * \alpha^2 * Y_2 * R_W = 2\pi R_X \quad (24)$$

Where, K_{Vd} is the orbiting cycles that each of these orbs (or the points of any P_d) performs, in T_X, in order to travel a distance equal to P_X of Cs_{24+4}, and thus it conserves ω_x of the system. For Earth, K_{Vd} is about 192 cycles; accordingly, T_X of our solar system is 192 Earth-years[iii].

For ion-carrier-orbs, as Venus and Mercury, their spin-equations could be formulated as follows. Since, $V_d^2=2\pi^*K_{Vd}$, we can write Eq.20 in the form of Eq.25.

$$K_{Vd}^2 * 2\pi Pd = P_X \qquad (25)$$

If we imagine that, the ion-carrier orbs are in the ready state as the orbs of a *Bs*, before the moment of carrying, we get Eq.26.

$$\alpha * P_o = 2\pi P_d \qquad (26)$$

Then, we can substitute the quantity ($2\pi Pd$) in Eq.25 with the left side of Eq.26. Besides, when these orbs become actually loaded with a base of a *Bs* (as an ion), their domain and steering thrust becomes *X* of that orb-less *Bs* instead of P_o; thus, the orbiting-spin-equation for the ion-carrier orbs of Cs_{24+4} is as follows.

$$K_{Vd}^{2*} \alpha * X = P_X \qquad (27)$$

[iii] In the ancient Egyptian architectonic records, T_X= 195 Earth-years; and $26T_X$ (5070 years) is the cycle of Armageddon (Hor-Maged-don), or ¼ the time of earth's obliquity range.

Eq.27, shows that the ion-carrier-orbs also conserve ω_x in their motions; besides, as $K_{Vd}*P_d=P_X$, $X=2\pi R$, and $P_d=2\pi R_d$, we get Eq.28.

$$Px * \alpha * X = P_d^2 \qquad (28)$$

Then, the spin equation for the ion-carrier orbs of Cs_{24+4} is as follows.

$$Rx * \alpha * R = R_d^2 \qquad (29)$$

We know from section-2 that R_X (or R_{Zc}) of our solar system most probably equals 28,689 million km. Using NASA's planetary fact sheets [16b], R_d for Venus and Mercury is 108.21 and 57.9 million km, respectively. Their observed α is 1.924 c/T_d, and 0.5 c/T_d, respectively, i.e., α of these two planets is taken equal to the result of subdividing the "tropical orbit period" by the "length of day". Then, from Eq.29, R for Venus and Mercury is 0.212 and 0.234 million km, respectively, and accordingly their X equals 1.33 and 1.47 million km, respectively, taking into consideration that each of these planets has an X that differs from, and being less than, X of our solar system. Most probably, X of our solar system equals 5.88 million km for M_b equals 1.0 million-km. Hence, in relation to T_X, the T_b of X of our solar system is about 14.3 Earth-day. Besides, X of a Bs may be of any value, denoting a musical note; X for Venus and Mercury is equivalent to 1/100 the frequency of the musical-notes: Do_2 (C_2) and Re_2 (D_2), respectively, while, X of our solar system is 1/100 the frequency of the note Re_4 (D_4). If the spin data of these two planets are incorrect and their X were the same as X of our solar system, we may say that these two planets might be part of the surplus of HESBs of the Bs_2s that have not yet leave the system.

Concerning the spin of a nucleus of a *Cs*, e.g., our Sun, as said earlier, the system's nucleus carries the mean orbital moment that applies on the system during the ready-state, i.e., it carries the load length of the thrust that the frequency of its mean radius equals half ω_x of the system. In our solar system, half ω_x= 0.5*5.88= 2.94 c/T_X. Then, by using Eq.6, R_d for that different architectonic frequency ω_d is equal to 1,793*10^6 km. Hence, the spin of the Sun α_n in T_X (192 Earth-years) equals the result of subdividing the perimeter of that median thrust by the equatorial-thrust's perimeter of the Sun, i.e., α_n=2π(1,793*10^6)/2π(696*10^3)= 2576.14c/T_X; then, 2,576.14/192 gives 13.41 c/Earth-year. Here, each cycle is about 27.22 Earth-days, which matches the observed spin of the Sun, in NASA fact sheets [16b].

Furthermore, one can imagine that natural satellites (e.g., Moon and Titan) are as orbs of a carried *Bs*; and thus they will not participate with other basic systems for assembling a *Cs*. Therefore, they are, in the sleeping mood, and most likely, they do not spin. Due to this, I imagine that each natural satellite has a fixed orientation towards its system's nucleus (planet), and as known, the day of each is equal to its orbiting period. I can also imagine that the system of Earth and Moon is like a Bs_1 that is carried on one of the orbs of Cs_{24+4} (our solar system). Thus, our planet Earth may be an HESB and our Moon may be the orb of that Bs_1. As mentioned in section-1, an HESB is composed from a male solid core inside a female spherical-shield (may be the terrestrial Atmosphere)[iv].

[iv] The ancient Egyptians depicted this basic principle in cosmic structure in their temples and tombs, i.e., they depicted earth like a man, and depicted the sky like a woman surrounding the earth.

Section-4.
Gravitation and Music of the Spheres

In Eq.21, since, V_d is cycles that the architectonic angular velocity of each is 360°, then, V_d may represent the velocity of any point on the thrust P_d in any given time scale. Eq.21 implies that as the radius R_d increases, V_d reduces; and when R_d equals R_X, V_d^2 equals 2π. In our solar system, R_d equals V_d^2 at nearly the median circle of the asteroid belt, where it is the neutral path of Cs_{24+4}. Here, V_d is the product of the load that applies on its thrust due to the four directional motions of Cs_{24+4}, and R_d is the altitude of the floor-level of that load. The neutral path differs from the path of the mean orbital moment; the latter is due to the ready state of the system, i.e., the system is ready to join with, or to carry other, systems, using its unloaded orbs that run, and could be found, near to its P_{dM}. The radius of the neutral path R_{NP} of our solar system could be given by $R_{NP}^2 = R_d * V_d^2$. Where R_d and V_d are the mean orbital radius (in million km, which equals M_b) and the orbital velocity (per Earth-second) of a diverse (any) planet in our solar system, respectively.

Moreover, since V_d^2 times R_d of any P_d in Cs_{24+4} equals $2\pi R_X$, the correlation between the velocities of two orbs (V_{d1} *&* V_{d2}), in any given time-scale, and the mean radii of their diverse thrusts (R_{d1} & R_{d2}) could be reckoned using Eq.30.

$$V_{d1}^2 * R_{d1} = V_{d2}^2 * R_{d2} \qquad (30)$$

If we substitute the radii in Eq.30 with their values from Eq.6 ($R_d=24\omega_d^4$), we get the correlation between the velocities of two orbs and the imaginary architectonic frequencies of the radii of their diverse-thrusts.

$$V_{d1} * \omega_{d1}^2 = V_{d2} * \omega_{d2}^2 \qquad (31)$$

Eq.31 implies that, in our solar system, the velocity that corresponds to 1/100 of ω_d= La_2# of 117c/T_b (i.e., at 45 million-km from sun's center) will be 4 times the velocity for its second harmonic: 1/100 of ω_d=La_3# of 234c/T_b (at 720 million-km from sun's center). Increasing ω_d by one octave means its quantity became double, its R_d increased up to 16 times, and its V_d reduced down to its 1/4. Eq.30 and Eq.31 together constitute the architectonic harmonic-law of traveling in a steering ethereal structure-SES, which now I imagine and can say it is composed from the thrusts of rings (the harmonic ethereal fibers). I expect that this law should work not only in Cs_{24+4} but also in any *Cs* or *Bs* in the cosmic enclosure, no mater what its order or size is.

Since SES is the plane of the equatorial thrusts of any system, and each of these thrusts is an equator of a harmonic sphere that its surface is built by multiple thrusts parallel to its equatorial plane, as latitudes, Eq.30 and Eq.31 also link these latitude-thrusts. Taking into consideration that the velocity of latitude-thrusts of any orb in Cs_{24+4} in T_X is constant, due to conserving ω_x. Moreover, we can also say, because spherical orbs, and perhaps any celestial body, are shaped primarily by an array of parallel and semi-elliptic-thrusts, they are not perfect balls.

Linking the architectonic-law of traveling in SES of two systems, where one of them carries the other, e.g., SES of Cs_{24+4} and SES of any of its system carrier orbs (e.g. planets) needs the following discussion. Since, the orbs are running on, and partly steered by, what looks like an imaginary musical strings, I presume that they resonate and transfer their orbits' velocities V_d to the initialization or index-thrust of their systems that upon which the velocity of a point on any thrust-curve in the orb's system can be reckoned using Eq.30. Based on reviewing the published data in NASA planetary fact sheets concerning the observed velocities of natural satellites of planets [16c], I found that the index-thrust of Earth, Mars and Pluto is P_{ZZ} (equals $2\pi P_Z$) of the main thrust of a contour level of the steering mechanism. However, for planets of the second octave of Bs_2s' rings, excluding Jupiter, P_3 was their index thrust. Then, for establishing their equations, the proposed contour-levels contain the following thrusts: (P_{Z3}-P_3-P_{M3}), (P_{ZZ2}-P_{Z2}-P_2-P_{M2}), (P_{ZZ1}-P_{Z1}-P_1-P_{M1}), and (P_{ZZ0}-P_{Z0}-P_0-P_{M0}).

Where, $P_{Z3}= S*P_{Z2} = S^2*P_{Z2}= S^3*P_{Z1}= S^4*P_{Z0}$.

And, $P_{ZZ2}= 2\pi P_{Z2}$, $P_{ZZ1}= 2\pi P_{Z1}$, and $P_{ZZ0}= 2\pi P_{Z0}$.

Upon this, we can put Eq.9 in the following form,

$$\alpha * P_{Z2}= (2\pi)^2 * P_3 \qquad (32)$$

Similarly,

$$\alpha * P_{Z1} = (2\pi)^2 * P_2 \qquad (33),$$

And,

$$\alpha * P_{Z0} = (2\pi)^2 * P_1 \qquad (34)$$

Then, from Eq.32, Eq.33, and Eq.34 we get Eq.35 and Eq.36.

$$\alpha^3 * R_{ZZ1}= (2\pi)^5 * R_d \qquad (35)$$

$$\alpha^4 * R_{ZZ0}= (2\pi)^6 * R_d \qquad (36)$$

Upon this, Eq.9 identifies the radius R_3 of the index - thrusts of Saturn, Uranus, and Neptune; Eq.35 identifies the radius R_{ZZ1} of the index-thrust of Pluto; and Eq.36 identifies the radius R_{ZZ0} of the index-thrusts of both Earth and Mars. However, I found that the radius of Jupiter's index-thrust R_{3-} equals

R_3 times the fourth root of 2π (=1.5832); i.e., it equals about 10 times of its $R_{M3.}$ If Jupiter's data is correct, it seems that there might exist some intervals between P_3 and $P_{Z3,}$ having the factors: $(2\pi)^{2/3}$, $(2\pi)^{1/2}$, $(2\pi)^{1/3}$, and $(2\pi)^{1/4}$. Thus, the equation of Jupiter's index thrust is,

$$\alpha^* R_{3-} = (2\pi)^{5/4} * R_d \qquad (37)$$

Using Eq.36, R_{ZZ0} for Earth equals 517km; then if we put in Eq.30 the velocity of R_{ZZ0} equal to V_d of the Earth (29.78 km/second), the velocity of the Moon's orbiting thrust that its mean radius equals 384,400 km would be equal to 1.06 km/second. Besides, using Eq.30, V_d for Jupiter (at R_d equals $778.56*10^6$ km), in relation to V_d of the Earth, equals 13.054 km/second. According to Eq.37, it is also the velocity of the index thrust of Jupiter that has a mean radius R_{3-} equals 739,003km. Then, using Eq.30, the velocity of Callisto's thrust that has a mean radius equals 1830,000 km is about 8.29 km/second. For Mars, using Eq.36, its R_{ZZ0} is equal to 68.49km and according to NASA's planetary fact sheets [16b] its V_d=24.13 km/second, then, using Eq.30, the velocity of the thrust of Phopos is 2.06 km/second and the velocity of the thrust of Deimos is 1.30 km/second. Furthermore, I expect that, as V_d of a planet (or an orb) changes during its orbiting motion, due to the change in the load vectors between the perihelion and the aphelion of its P_d, the velocity of any point of the index-thrust of the planet would also change. Hence, the velocities of thrusts of a planet's system (a loaded-orb) will also change during its T_d. Thus, a natural satellite will have different orbiting time for each cycle of it during the T_d of its home planet.

Based upon what have been said, the steering motions in Cs_{24+4}, are the motions of the main *X*-thrusts of each contour level of both the harmonization and the steering mechanisms of a system-carrier-orb that are namely: P_o, P_1, P_2, P_3, P_d, P_E, P_F, and P_{Zc}. As thrusts, they represent seven motions plus the four hidden motions of P_{Zc}, hence, the steering motions for each loaded or unloaded orb, e.g., a planet, are 11 at most; we observe only two of them.

Moreover, for the system-carrier orbs, we can assume that their M_b equals 100 km, i.e., it equals 10^{-4} of M_b of Cs_{24+4}; I use 10^{-4} as a reduction interval between M_b of the mother system and M_b of its subsystems, since the mother system is of the fourth order. Accordingly, Eq.6 could be used to get the imaginary architectonic frequency of any radius in the systems of orbs (e.g., planets' systems), as they take place within the jurisdiction of Cs_{24+4}.

Now, according to the *Newtonian* law of gravitation, the escape velocities from planets in our solar system have been identified [14, 15]. Using Eq.30, we can identify, for each planet, to which thrust of its system the escape velocity belongs. I found that the escape velocity is related to a thrust in the planets' systems that the imaginary architectonic frequency ω_d of its mean radius is 1/100 of the musical note La_2= 110c/T_b or its first harmonic La_1= 55c/T_b, as M_b=100 km. The former is ω_d for the radius 3,514 km, and the latter is ω_d for the radius 219.6 km.

For Earth, using Eq.30, in relation to its index thrust, the velocity of that *La*-110-thrust is 11.42 km/second. For Mars, the velocity of the thrust that its radius equals 2π the radius of *La*-55-thrust, at 1,379 km, is equal to 5.37 km/second. For Jupiter, the velocity of the thrust that its radius equals $(2\pi)^{5/4}$ of *La*-110-thrust, at 34,956 km, is about 60 km/second. For Saturn, the velocity of the thrust that its radius equal 2π of *La*-110-thrust, at 22,079 km, is about 39.78 km/second. For Uranus and Neptune, if their data is correct, the velocity of the thrust that its radius equals $(2\pi)^{2/3}$ of La-110-thrust, at 11,819 km, is about 22 and 24 km/second, respectively; however, if they are similar to the case of Saturn, their escape velocities at 2π of *La*-110-thrust will be 16.11 and 17.61 km/second, respectively. For Pluto, the velocity of the thrust that its radius equals $(2\pi)^{1/2}$ of *La*-55-thrust, at 559 km, is 0.91 km/second.

On rings of planets, likewise, we can presume that each system-carrier-orb, in Cs_{24+4} or any Cs, as a sub-system (e.g. a planet), has its protecting rings that form its equatorial disk, and similarly the corresponding array of orbs. For, I shall presume that, in our solar system as Cs_{24+4}, the planets' rings have the following order from the planets surface: 4 rings correspond to Bs_4 of Cs_{24+4}, one ring gap, 12 rings correspond to Bs_3s of Cs_{24+4}, and 3 rings as a cover for the planet's system. The cover of each is one level below the cover of Cs_{24+4}. In total, they are 20 rings or 20 diatones. Accordingly, with reference to Eq.6 and Eq.4, the radius of the system-carrier-orb's perimeter of the same is about $((2^{1/12})^{20})^4 * R_W$ = $(101.5936673*R_W)$. In our solar system, this number was assumed by scholars as 100 times the planet's equatorial radius. Upon this, I found that the observed rings of some planets take place within the limits of HMT of the combined ring of the planet's system. With reference to Eq.6 and Eq.4, the radius of the perihelion R_{PH} (lower-limit) of HMT of the combined ring for any planet is $(101.5936673*3^{-4}*R_W)$ that equals $(1.254242806*R_W)$; or as assumed it is $(100*3^{-4}*R_W)$ that equals $(1.234567901*R_W)$; where R_W in the latter is the planet's equatorial radius. Perhaps, the difference might be is in value of the factor Y, see section-3.

In addition, some observed rings start close to the neutral path of the planet's system, similar to the asteroid belt of our solar system (Cs_{24+4}), i.e., at the thrust that its mean radius R_{NP} equals to square the velocity of that radius, $R_{NP}=V_{NP}^2$. Thus,

$$R_i * V_d^2 = R_{NP}^2 \qquad (38)$$

Where, V_d is the orbiting velocity of the planet in second, and R_i is the radius of the index thrust of the planet (R_3, R_{3-}, R_{ZZ1} or R_{ZZ0}) in 100 km that = M_b of the planet; and R_{NP} will be in 100 km. Using Eq.38, R_{NP} of Jupiter equals 1,122.18 hundred-km (112,218 km); however, its R_{PH} equals 88,148km. R_{NP} for Saturn is 59,110km, but its R_{PH} equals 74,404km. R_{NP} for Uranus is 23,937 and its R_{PH} equals 31,554km. R_{NP} for Neptune is 26,166 and its R_{PH} equals 30,572km.

Furthermore, since natural satellites are orbs in the sleeping mood, most likely they do not spin. However, based on reviewing the data of satellites in our solar system, due to that, they have different working and orbiting radii for the same planet, as the case of Jubiter [16c], I think they are orbiting the nuclei (planets) of their systems based on a mutual zero-load-relation. For this, one can imagine that a natural satellite is a nucleus of a *Bs*, where its own equatorial perimeter P_{WS} is the module M_b of that *Bs*. Besides, the thrust *X* of that *Bs* has an imaginary architectonic frequency ω_{La} that always being the note *La* of any musical octave, e.g., La_2#110, La_3#220, La_4#440, or La_5#880 cycles/*s*, or above. If we imagine that, a natural satellite carries its home planet that is located on P_Z of the natural satellite's system, the load of the orbiting moment that is represented in travel distance by that P_Z would be equal to the load of the orbiting thrust of the natural satellite. Therefore, a natural satellite does not carry any load and accordingly it becomes in the sleeping mood. Then, the load vector R_Z of the satellite's system equals to the mean orbiting radius of the satellite. Thus,

$$R_{WS} * \omega_{La} = R_{dS} \qquad (39)$$

Where, R_{WS} is the mean equatorial radius of the satellite, R_{dS} is its mean orbiting radius, and ω_{La} is the architectonic frequency of a *La* note, or close to it. For Earth, the corresponding frequency of *X* of the moon's system is La_3#220 c/T_b. For Jupiter, ω_{La} for Callisto, Ganymede, Europa, and Io are about La_4#440, La_3#220, La_3#220, and La_2#110 c/T_b, respectively. The rest of natural satellites in our solar system have similar cases, even, those that are only Cs_{24+4}'s derbies like Phopos and Deimos of Mars. In most cases, ω_{La} of *X* of the satellite is 100 times ω_d of the *La*-thrust that is below ω_d of the mean radius of the satellite's orbiting-thrust. For Earth, ω_d of the Moon's orbiting-thrust[v] is 3.55 c/T_b; and 1/100 of

[v] If R_{dS} is in millimeters, the mentioned architectonic frequencies will be 355 c/T_b, and 220 c/T_b; where millimeter is 10^{-4} decameter.

the frequency of the *La* note below it, is 2.2 c/T_b; where R_{dS} is in 100Km.

Based upon the postulation behind Eq.39, I shall attempt to answer the question: what escape velocity implies, form the architectonic point of view? I can say, it is the state at which, the travel length of any point on the equatorial thrusts P_Z, X and P_M of a body standing on a planet's surface becomes perpetually equal to the travel length of 2π the thrust that to which the escape velocity belongs, in T_d of this thrust. If a body reaches this state, I expect it will be able to propel itself up to the perimeter of zero-load of that thrust in order to become in the sleeping mood while orbiting the planet at that height (altitude). For Earth, 2π the radius of its *La*-110-thrust is: $(110^4*24)*10^{-6} * 2\pi$ = 22,078 km. Thus, I imagine that, any point on the thrusts P_Z, X and P_M of a body that its R_Z=1.0 meter, should perform 255, 1,605, and 10, 088 c/second, respectively, in order to be able to propel it self up to that zero-load orbiting thrust. This body has a radius equal to R_M (2.53 cm), and it will perform a spin equal to 1,605 c/second, while its three thrusts will keep performing the mentioned cycles until it reaches the sleeping mood level. We should take into our consideration that, in this postulated scenario, the motions of the contour thrusts of the body generate its spin and not the opposite. Perhaps, here lies the secret of the architectonic attributes of the eternal ethereal systems, as

Plato wrote it might also be related to the form of the soul. If one was activated, it propels metals.

The other possible scenario is that the body in the mentioned example will be as an orb in the ready state. As mentioned in the previous sections, each thrust represents an *X* of a separate system while it still part of the mother-system that to which it belongs and both the thrust *X* and its P_Z have the same angular velocity. Then, this body will be free to go to the P_Z of *La*-110-thrust. Similar to an orb in the ready state, the body will, imaginary, go to that P_Z in order to carry other system and return to a lower thrust that its load equals the load of the system that the body has carried. However, due to that, the body was sent to that P_Z in an improper time, it would find nothing to carry, and because the body in our example is not a real orb of a Bs_1 or above.

Besides, as said earlier, if it was so, the orb of a *Bs* that was hosted within Cs_{24+4} via the capturing process of carrying will no longer be in the ready state as our Moon. Thus, the body will go for a long sleeping mood on that P_Z. Add to this, if this body was a real orb of a *Cs*, where it is located at, and move on its P_{dM}, and due to any external factor was sent in an improper time to the P_{Zc} (or P_X) of its system, I expect it will do the same as mentioned above. If this process occurred again to send it in an improper time to the system's P_{ZZc} (or P_{ZX}) or far beyond it, and was lost for any reason, we can say as known the system has become in a state of ionization.

Furthermore, if we imagine that our solar system is as a *Bs* (Bs_{24}), that its P_{dM} and P_{ZX} are similar to *X* and P_Z of that *Bs*, then the rest of the 24 orbs of our solar system will be orbiting near to its P_{dM}; i.e., the centers of their thrust-drivers are moving (sliding) on P_{dM}. They are in a ready state for capturing and carrying any *Bs*, passing near to P_{Zc}, adding a new planet to the system. The orbs in the ready state, therefore, represent the future of their complex systems because they bring new worlds into them. We can also imagine that a black hole as a very giant *Cs*; its multi orbs in the ready state are capturing every passing by system. Using the notion of *Einstein*, if our solar system has been captured by a black hole, our world will be then the future of that black hole. However, if two *Cs* of similar order and size, e.g., two of Cs_{24+4}, have approached each other, it is expected that they would capture each other based on a mutual zero-load relation; each will then stand on the P_{Zc} of the other system, may be similar to the case of binary stars.

Now, we come to the most famous question: why bodies fall down, towards the center of a planet. Based on what I have postulated so far from the architectonic point of view, and following the postulation of *Plato*, all bodies in the cosmic enclosure, including all creatures, should have at least one contour level of the steering mechanism like a *Bs*: the main diverse-thrust X, the minor diverse-thrust P_M and the-same P_Z (or the-one). If a body stands on a planet's surface and cannot escape from it, it is neither in a ready state nor in a complete sleeping mood. Any body, according to its process of evolution and location, if it is not in a ready state, most likely, it will prefer to be in a complete sleeping mood similar to natural satellites. However, if this body is in a location that its contour-thrusts do not perform the needed cycles that enable it to propel itself up to the P_Z of *La*-110-thrust of its home planet, it will then prefer to go down one octave to P_Z of *La*-55-thrust at a radius equals 1,376km. Logically, it will prefer to go down to the thrust that its travel length is equal to the travel length of the three-contour-thrusts of its steering mechanism, per T_d of X (or $1/(2\pi)$) of that thrust, in order to be in a sleeping mood.

Based on this postulation, an asteroid might not hit our earth if the travel length of its contour thrusts where more than the travel length of P_Z of the *La*-220-thrust of the Earth. It might orbit the Earth instead, similar to the case Deimos and Phopos of Mars. Since, *La*-110-thrust of Mars is about 117 km above its surface, Phopos runs on nearly the P_Z of *La*-110-thrust and Deimos runs on nearly P_{ZZ} of *La*-

55-thrust of Mars. With this end, I comeback to where I have started. As *Plato* and his Italian colleague said [2], all motions of the ethereal/material systems in the cosmic enclosure are the output of one law, which is the harmonic tuning between a diverse-orbit and the frame of reference of its home system. That is, conserving the musical-note of the outer orbit that he named it the-same or the-one, and that to which a diverse-orbit belongs or within which a diverse-orbit of other invited-system is being temporally hosted.

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